WHAT IS CLAIMED IS:

- 1 1. An output power controlling apparatus for an internal
- 2 combustion engine for controlling operation of an output
- 3 power adjustment member based on a target torque
- 4 correlation value, comprising:
- 5 a vibration component prediction section for
- 6 predicting a vibration component to be generated on a
- 7 vehicle from the target torque correlation value using
- 8 a predetermined prediction model; and
- 9 a feedback correction section for feedback
- 10 correcting the target torque correlation value based on
- 11 the vibration component predicted by said vibration
- 12 component prediction section so as to suppress the
- 13 vibration.
 - 1 2. The output power controlling apparatus for an
 - 2 internal combustion engine as claimed in claim 1, wherein
 - 3 the predetermined prediction model is set based on a
- 4 transfer function of a second-order lag system.
- 1 3. The output power controlling apparatus for an
- 2 internal combustion engine as claimed in claim 1, wherein
- 3 said feedback correction section includes a control gain
- 4 variation section for setting a control gain to a higher
- 5 value in response to an increase of the vibration component
- 6 predicted by said vibration component prediction section.

- 1 4. The output power controlling apparatus for an
- 2 internal combustion engine as claimed in claim 1, wherein
- 3 the target torque correlation value is calculated based
- 4 on an accelerator opening, and said output power adjustment
- 5 member is controlled based on the target torque correlation
- 6 value after corrected.
- 1 5. The output power controlling apparatus for an
- 2 internal combustion engine as claimed in claim 2, wherein,
- 3 where a target vehicle attenuation coefficient is
- 4 represented by ζ' , an actual vehicle attenuation
- 5 coefficient by ζ , a natural frequency set in accordance
- 6 with a transmission gear ratio by ω_n , and a Laplace operator
- by s, the transmission function is calculated in accordance
- 8 with
- 9 $1/(s^2 + 2\zeta \omega_n s + \omega_n^2)$
- and a control gain K set by said feedback correction section
- is calculated in accordance with
- 12 $K = (\zeta' \zeta) \cdot 2\omega_n$
- 1 6. An output power controlling method for an internal
- 2 combustion engine for controlling operation of an output
- 3 power adjustment member based on a target toque correlation
- 4 value, comprising:
- 5 a vibration component prediction step of predicting
- 6 a vibration component to be generated on a vehicle from
- 7 the target torque correlation value using a predetermined

- 8 prediction model; and
- 9 a feedback correction step of feedback correcting
- 10 the target torque correlation value based on the vibration
- 11 component predicted by the vibration component prediction
- step so as to suppress the vibrations.
 - 1 7. The output power controlling method for an internal
 - 2 combustion engine as claimed in claim 6, wherein the
 - 3 predetermined prediction model is set based on a transfer
 - 4 function of a second-order lag system.
 - 1 8. The output power controlling method for an internal
 - 2 combustion engine as claimed in claim 6, wherein the
 - 3 feedback correction step includes a control gain variation
 - 4 step of setting a control gain to a higher value in response
 - 5 to an increase of the vibration component predicted by
 - 6 the vibration component prediction step.
 - 1 9. The output power controlling method for an internal
 - 2 combustion engine as claimed in claim 6, wherein the target
 - 3 torque correlation value is calculated based on an
 - 4 accelerator opening, and said output power adjustment
 - 5 member is controlled based on the target torque correlation
 - 6 value after corrected.
 - 1 10. The output power controlling method for an internal
 - 2 combustion engine as claimed in claim 7, wherein, where

- 3 a target vehicle attenuation coefficient is represented
- 4 by ζ' , an actual vehicle attenuation coefficient by ζ ,
- 5 a natural frequency set in accordance with a transmission
- 6 gear ratio by ω_n , and a Laplace operator by s, the
- 7 transmission function is calculated in accordance with
- 8 $1/(s^2 + 2\zeta \omega_n s + \omega_n^2)$
- 9 and a control gain K set by said feedback correction step
- 10 is calculated in accordance with
- 11 $K = (\zeta' \zeta) \cdot 2\omega_n$